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Space-Time Adaptive Processing Using Sparse Arrays

Michael Zatman

11th Annual ASAP Workshop

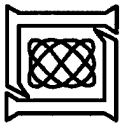
March 11th-14th 2003

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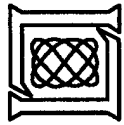


Application: Space Based Radar

Fast orbital velocity
(Large aperture ~
GMTI performance) →

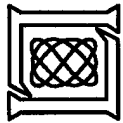
Long range to target
(Large aperture ~
location accuracy)

Launch cost
~low weight
and size (folded)

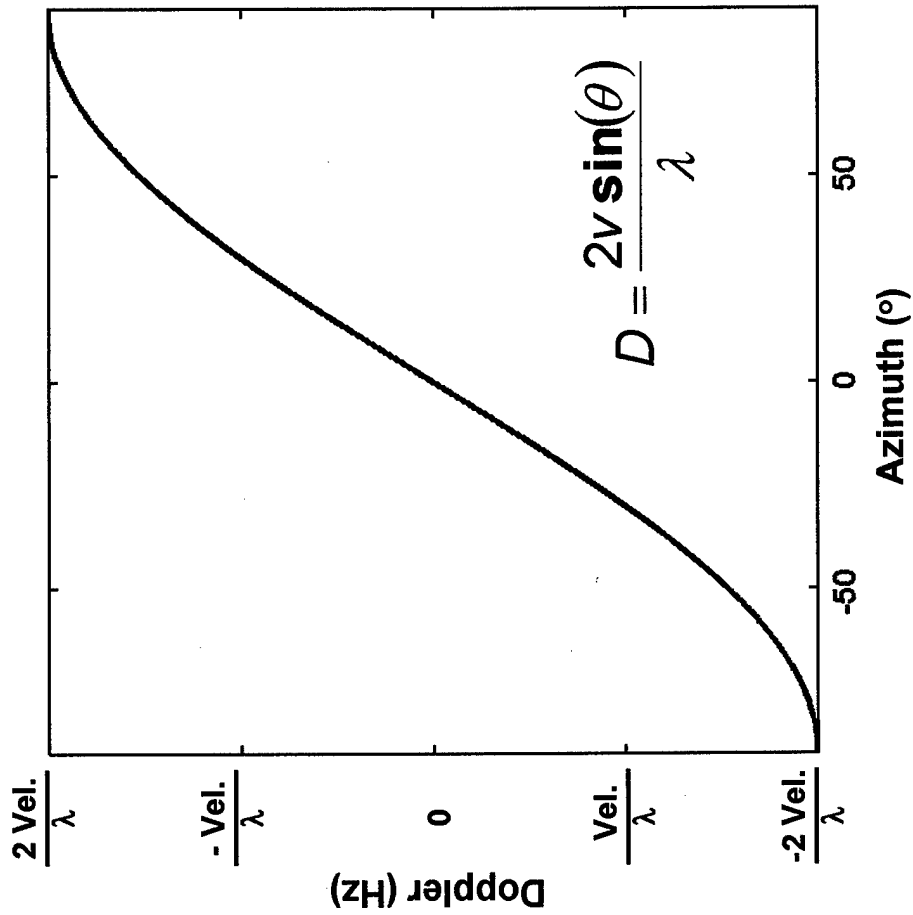
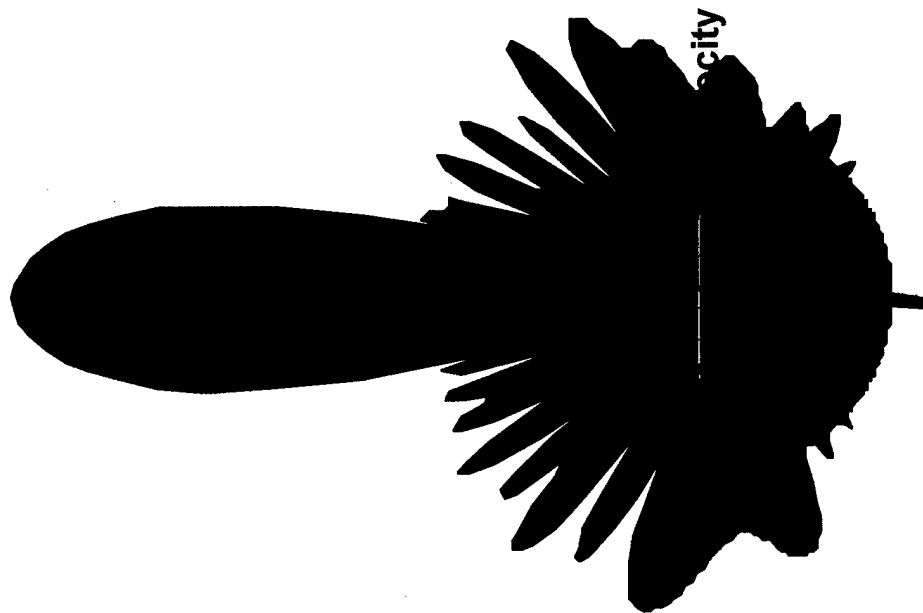


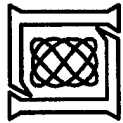
Outline

- Introduction
- Theory
- Performance
- Summary

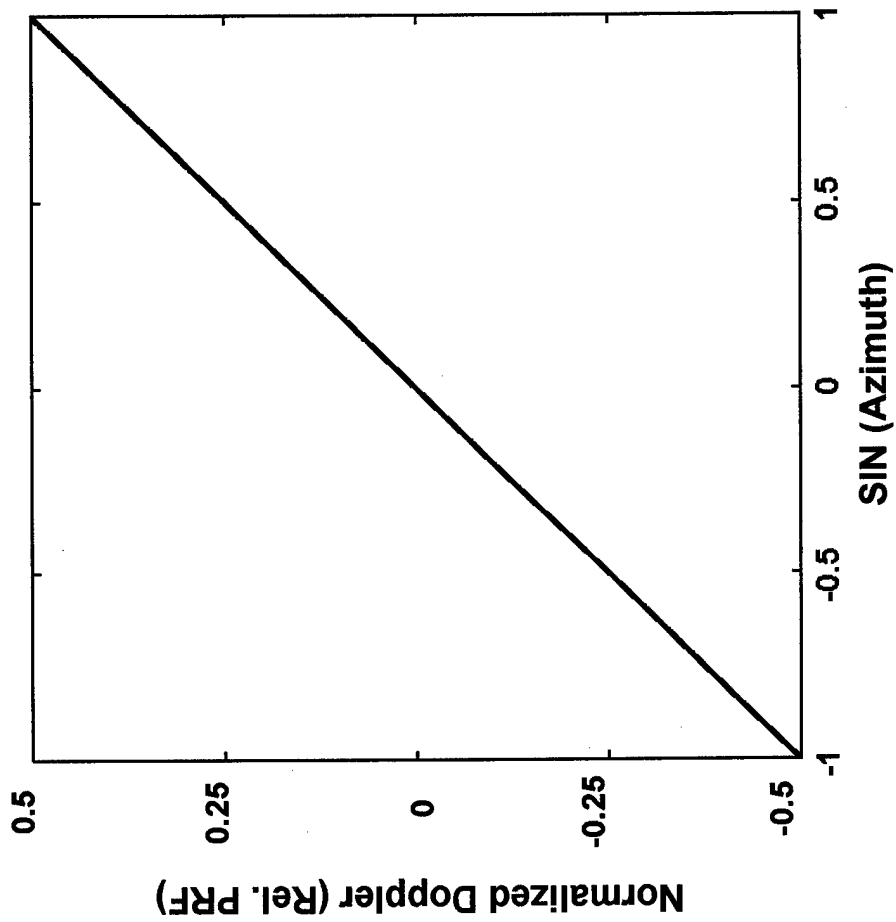
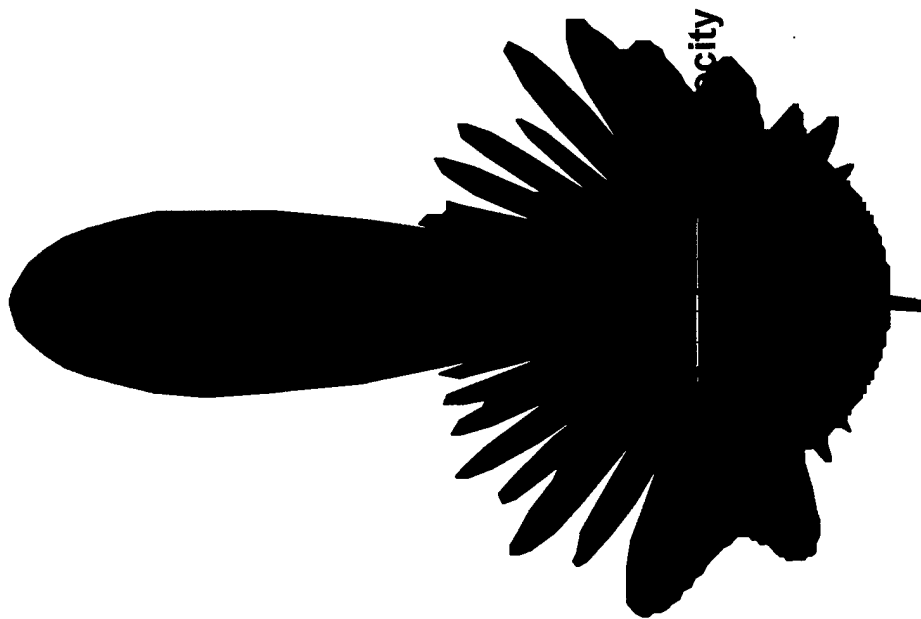


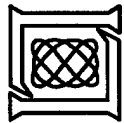
STAP Units



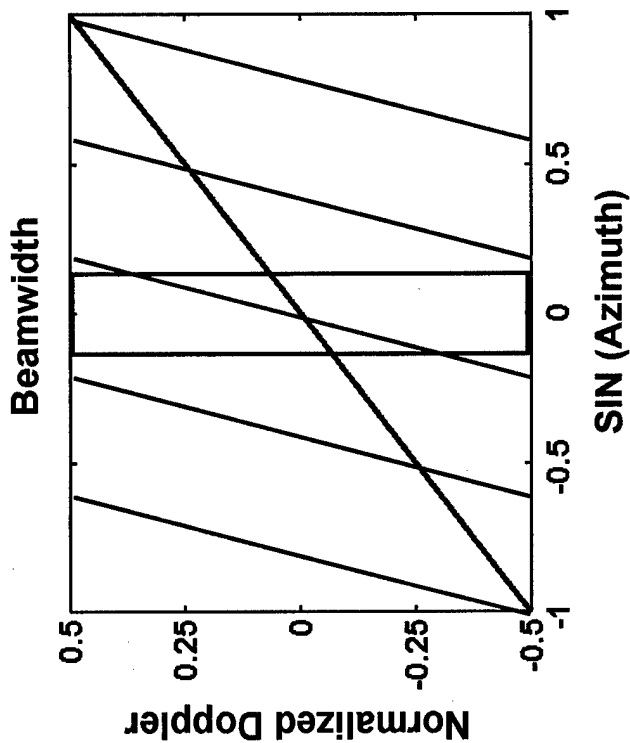


STAP Units





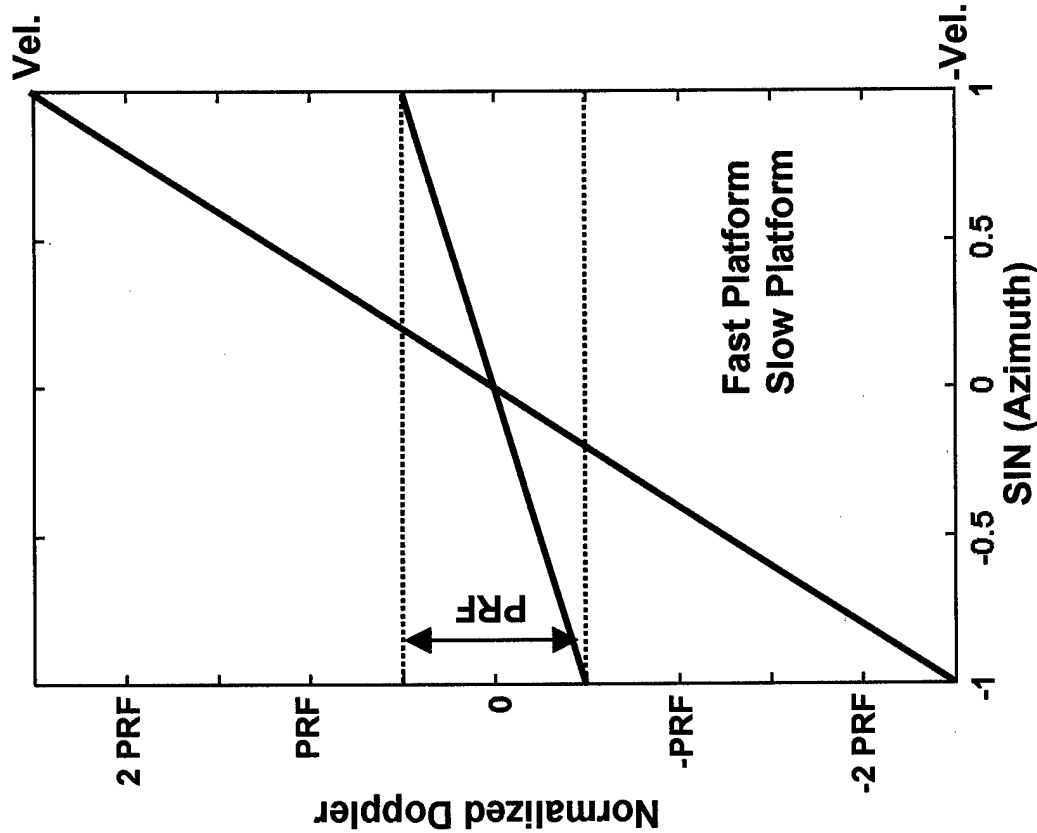
Doppler Ambiguous Clutter



$$\beta = \frac{4v}{\lambda PRF}$$

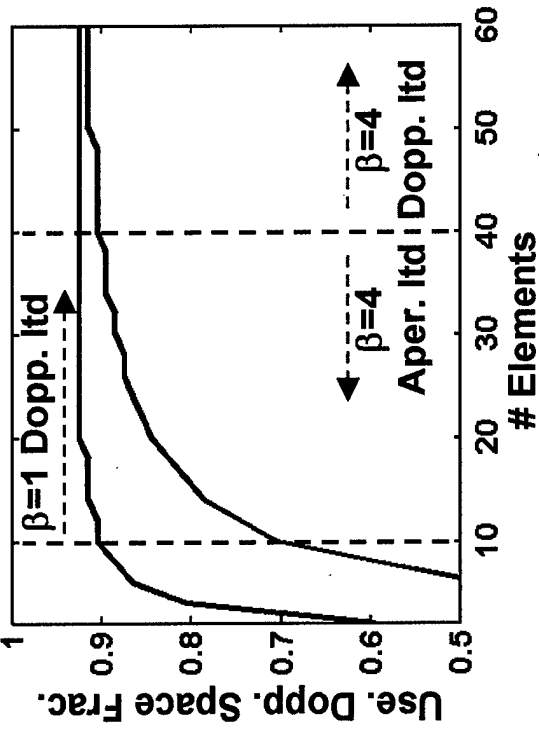
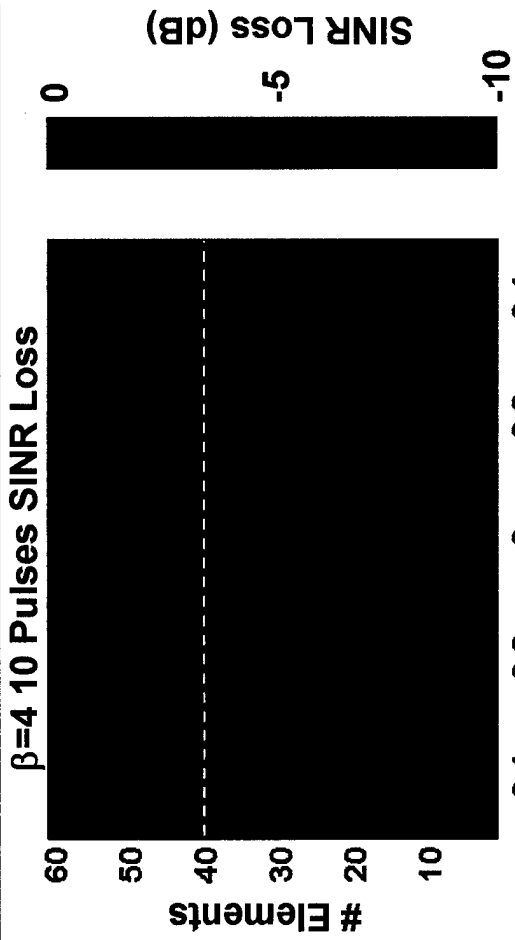
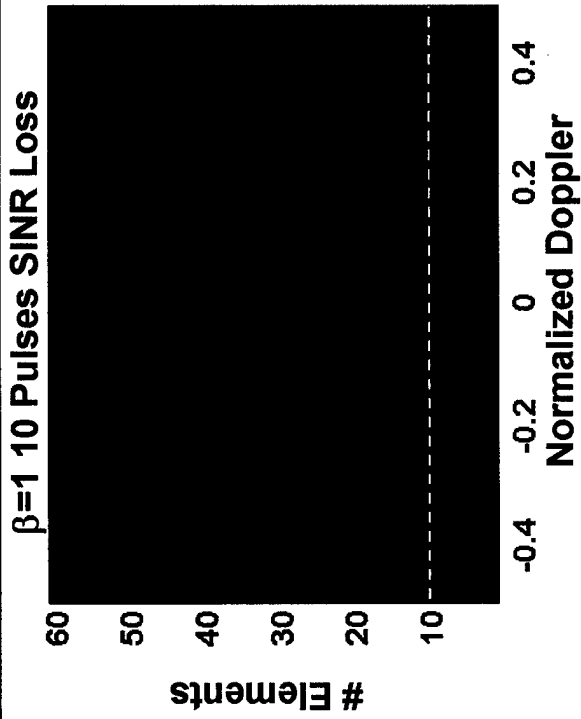
$$\text{Main Beam} = \frac{\lambda 2v}{L} \text{ (m/s)} = \frac{4v}{L} \text{ (Hz)}$$

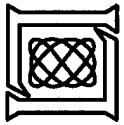
$$\text{Clutter Width} = \frac{4v}{L}$$





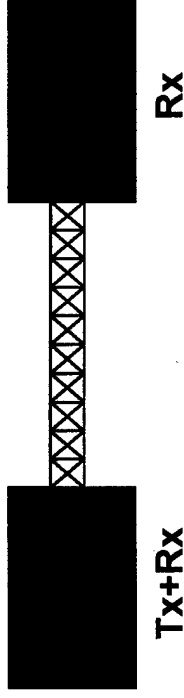
Aperture and Doppler Limited Performance



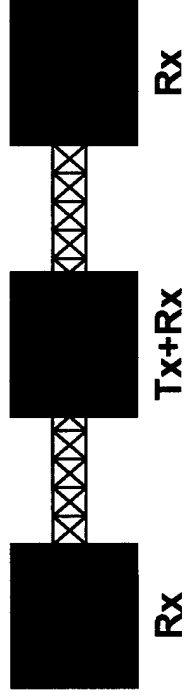


Some Sparse Array Concepts

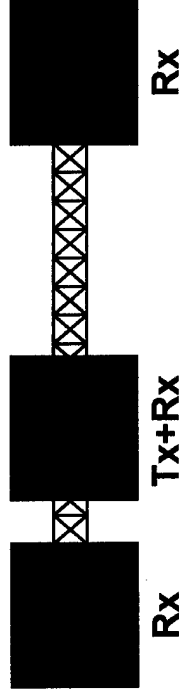
Interferometer



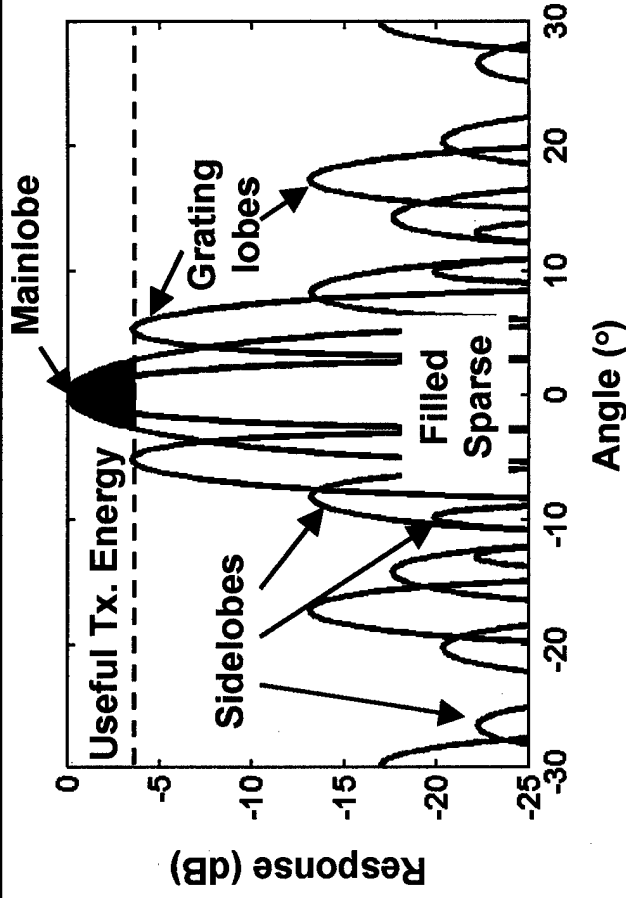
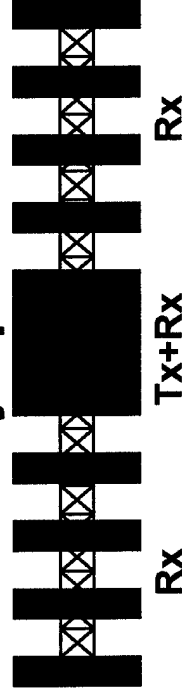
Even Spaced Equal Size



Uneven Spaced Equal Size



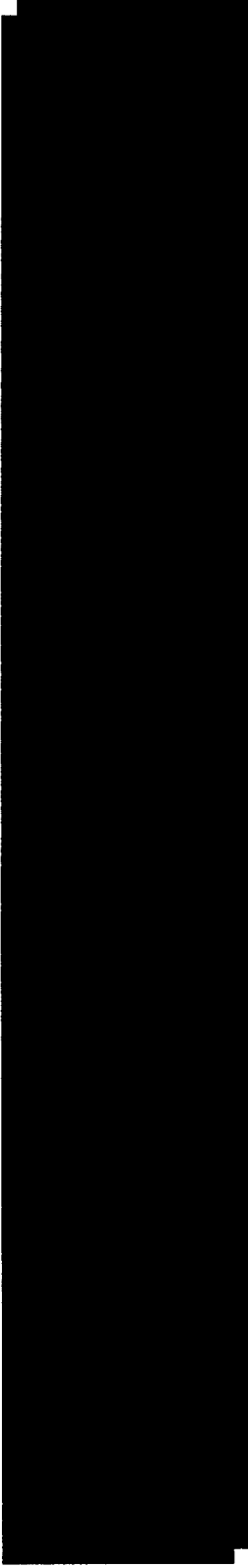
Many Apertures



- Sparse arrays trade mainlobe width against grating lobe height to find the optimum sparseness
- Energy transferred from the mainlobe to the grating lobes is useless for Tx.
 - Use a filled section of the sparse array for Tx. And form multiple Rx. beams

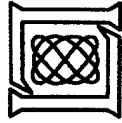


Sparse Array Issues



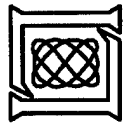
- Angle estimation performance
 - Improved accuracy due to narrower beamwidth (CRB)
 - Non-local errors due to grating lobes (WWB, ZZB, AB, ...)
- SAR performance
 - Multiple spatial samples per pulse
 - Tight PRF constraints
- Hardware and cost
 - Sparse arrays require less hardware
 - Cheaper & lighter

• ...

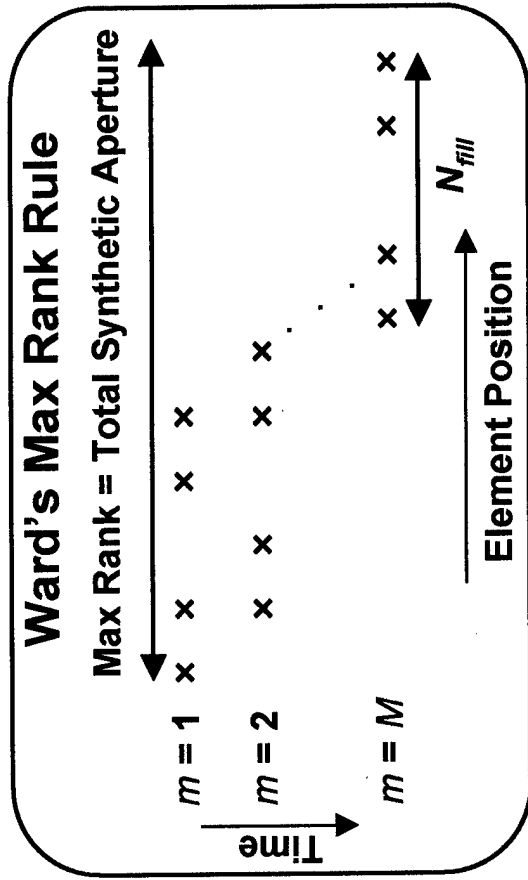
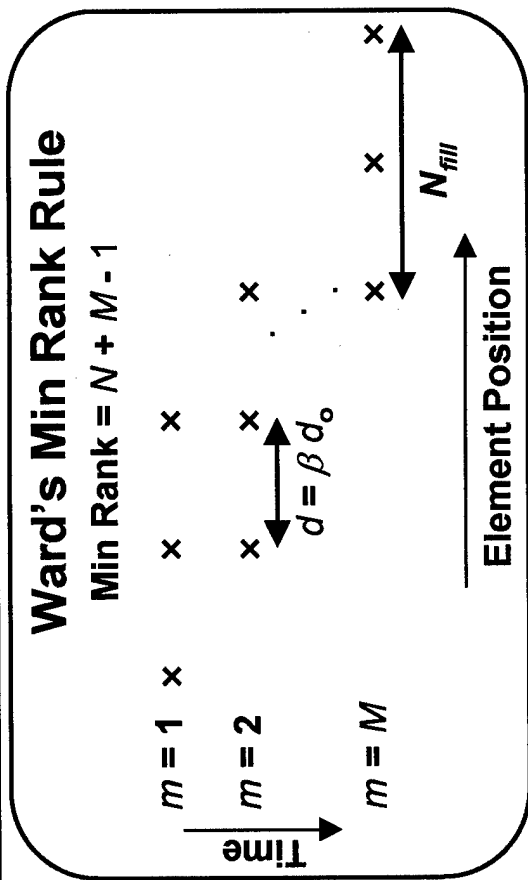
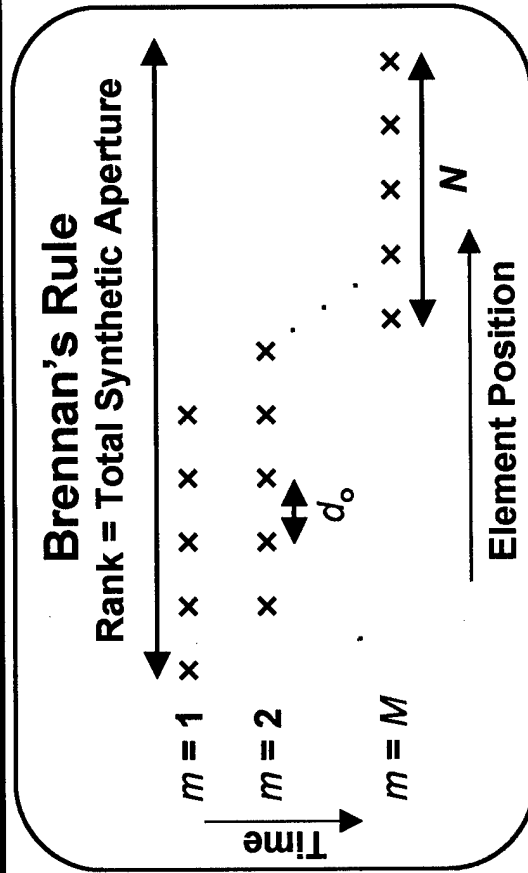


Outline

- Introduction
- Theory
 - Clutter Rank
 - Waveforms
 - SINR Loss
- Performance
- Summary



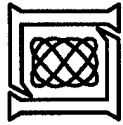
Brennan's Rule & Ward's Rules*



*J. Ward, Asilomar 1998

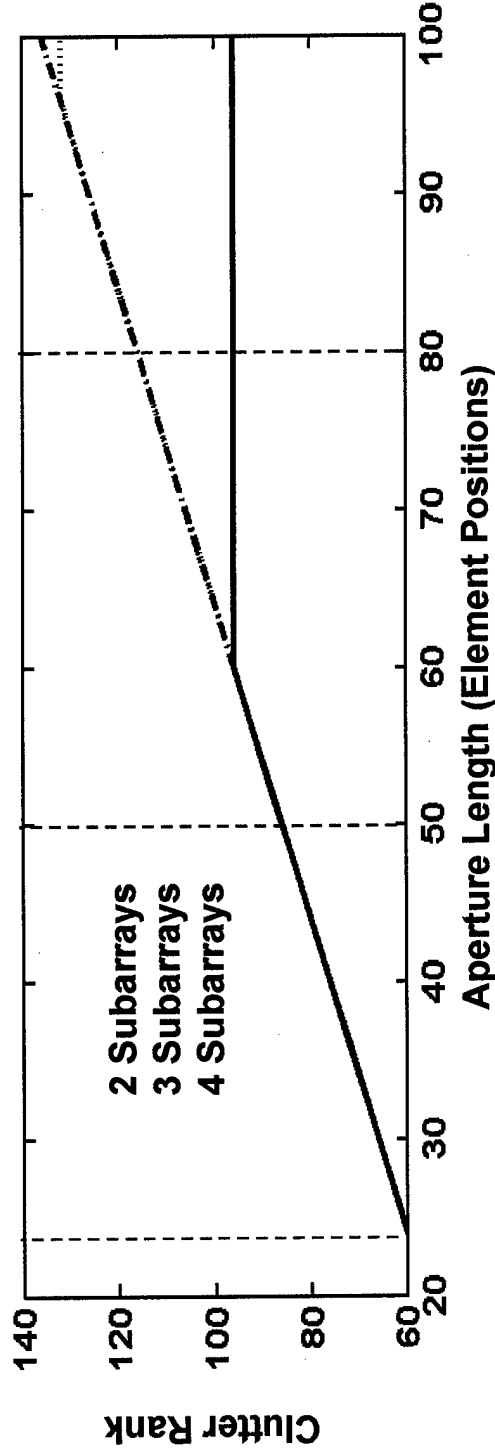
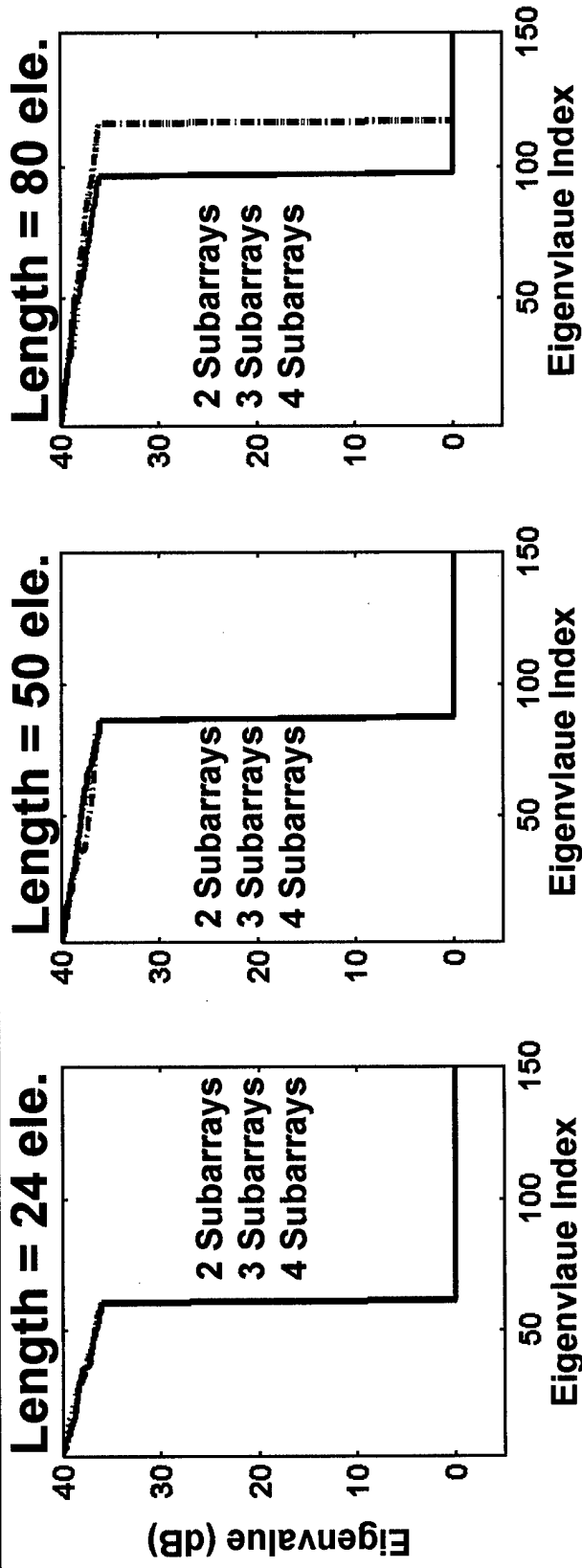
N = Number of elements, M = Number of pulses, $\beta = 2 \sqrt{T d_o^{-1}}$, N_{fill} = Number of elements in filled array

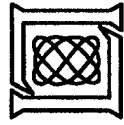
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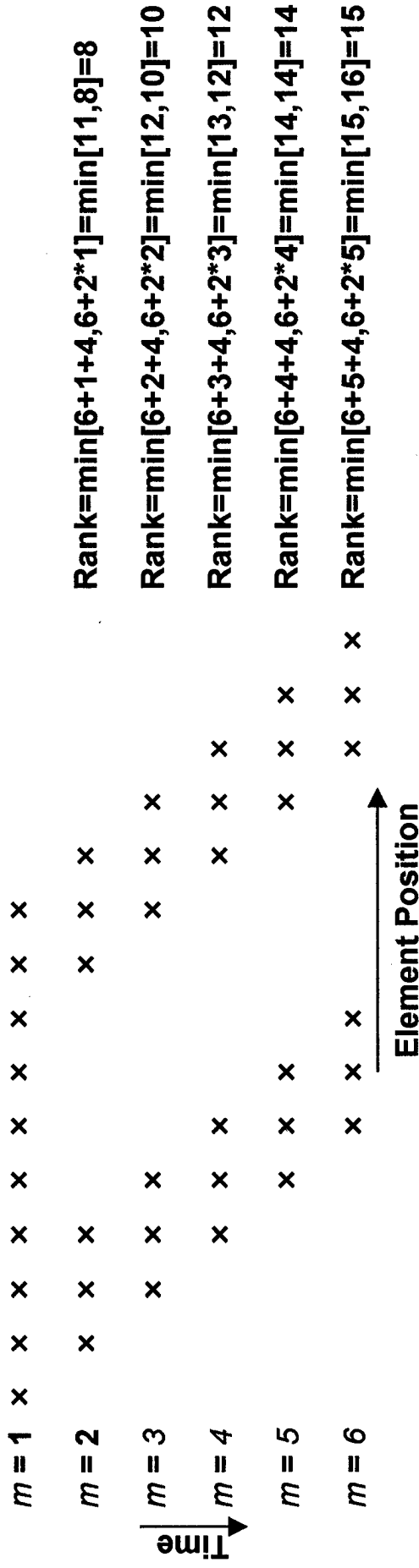
Additional Sparse Array Behavior

$N = 24$, $M = 10$, $\beta = 4$ Example





New (?) Rules for Sparse Arrays

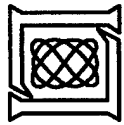


- For arrays which move less than the smallest subarray aperture during a pulse the rank is given by :

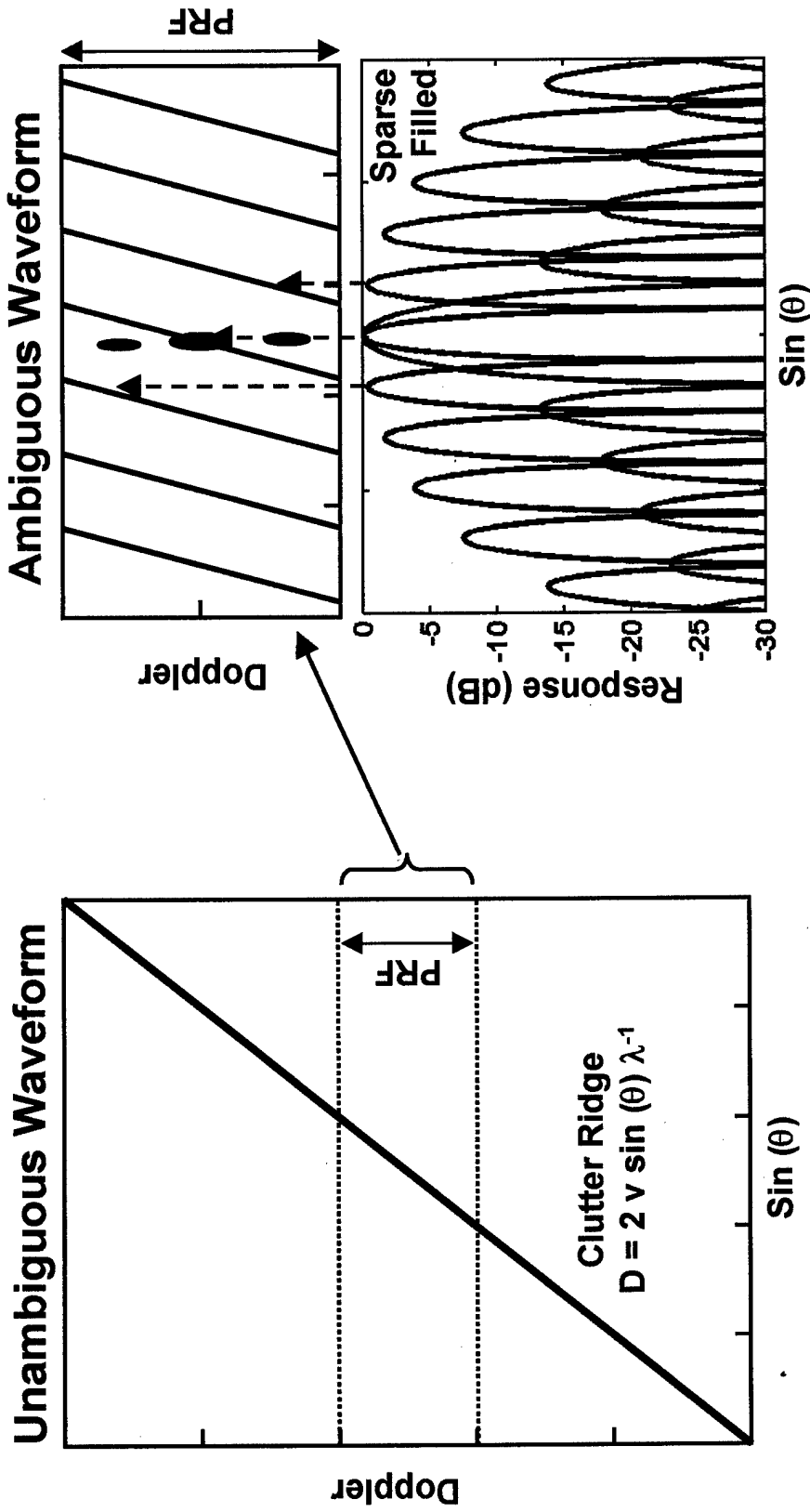
$$\min[N + \beta(M-1) + G, N + S\beta(M-1)]$$

Jim Ward's r_{\max} Using each sub array independently
- For equal size subarrays a sparse array is no better than a single subarray if

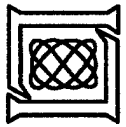
$$G > \beta(S-1)(M-1)$$
- I.e., The array is so sparse that there is no redundancy



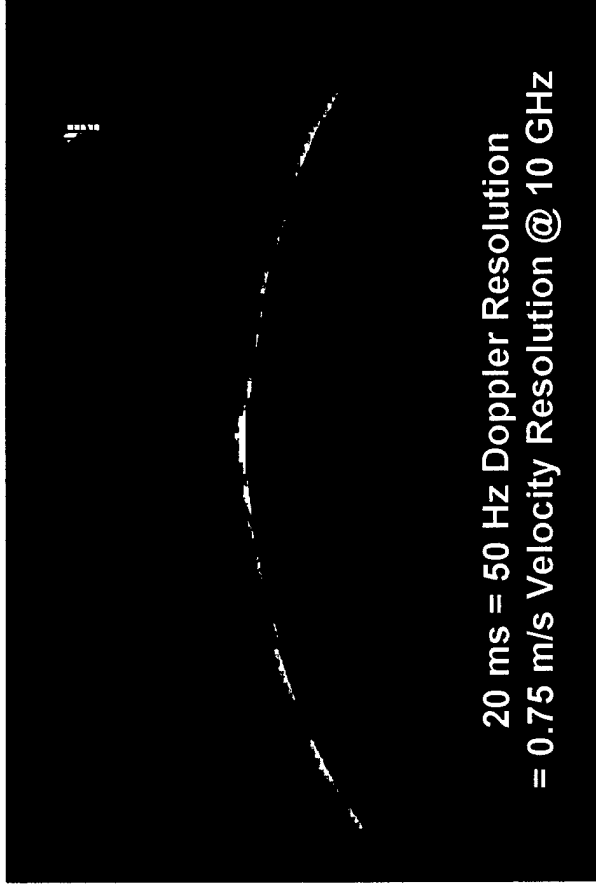
Sparse Aperture Waveforms



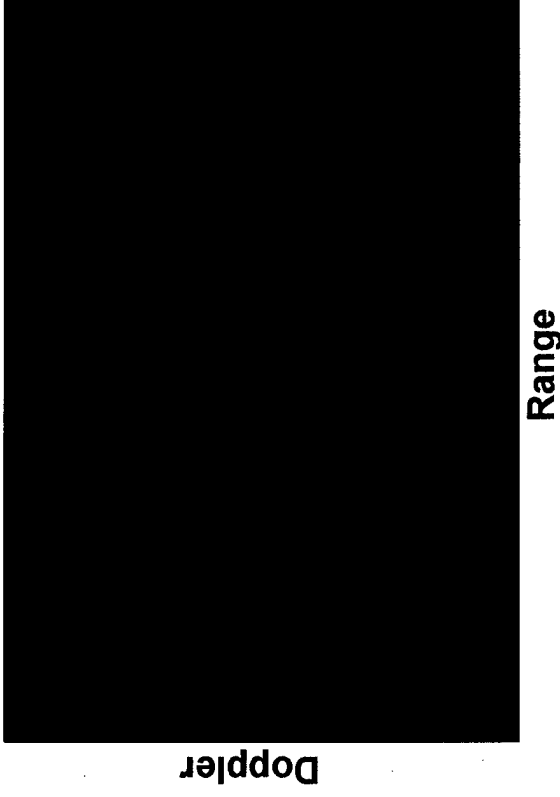
- Ambiguous waveforms (e.g., pulse-Doppler) and sparse (ambiguous) apertures lead to multiple clutter nulls
- Unambiguous waveforms preferable



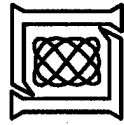
Long Single Pulse Waveforms



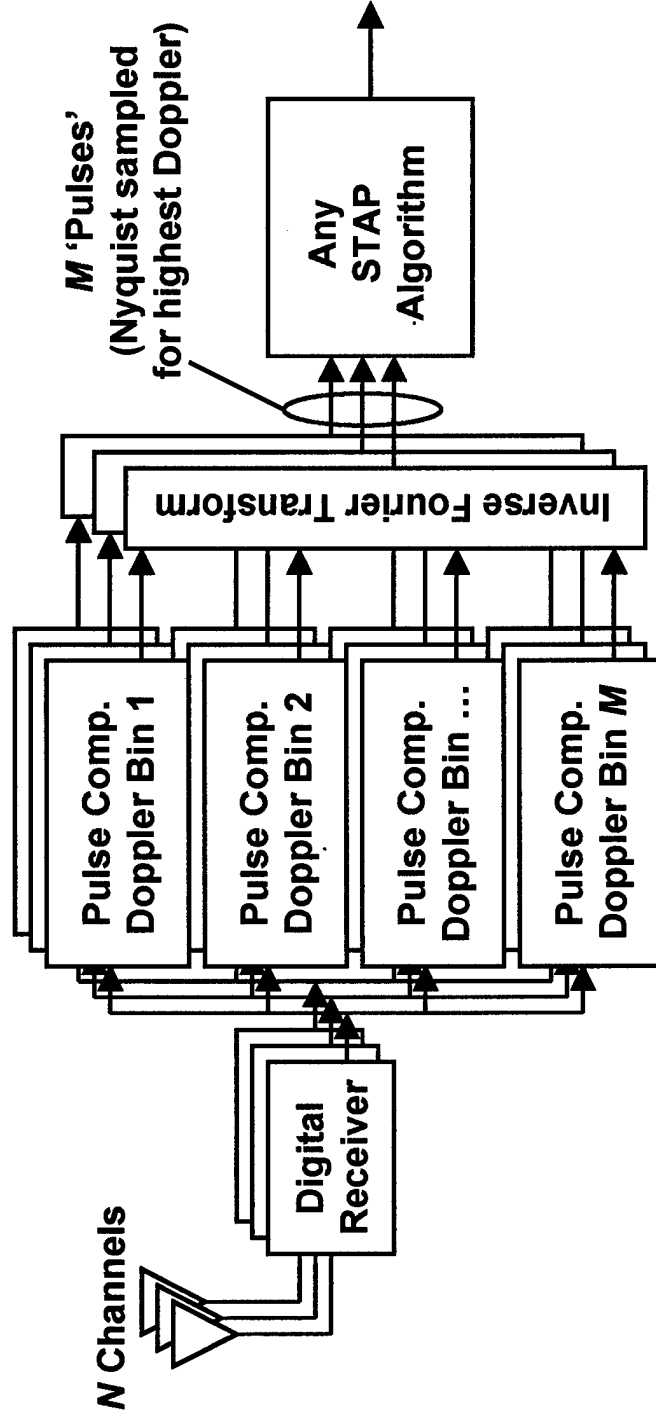
Phase Encoded Waveform



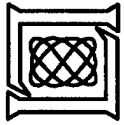
- Single pulse means no range or Doppler ambiguities
 - High chip rate sets Doppler ambiguities
- Must pulse compress each Doppler bin separately
 - More computation than pulse-Doppler waveforms
- Concern about strong sidelobe clutter > noise floor
 - Wide bandwidth & narrow antenna beam patterns



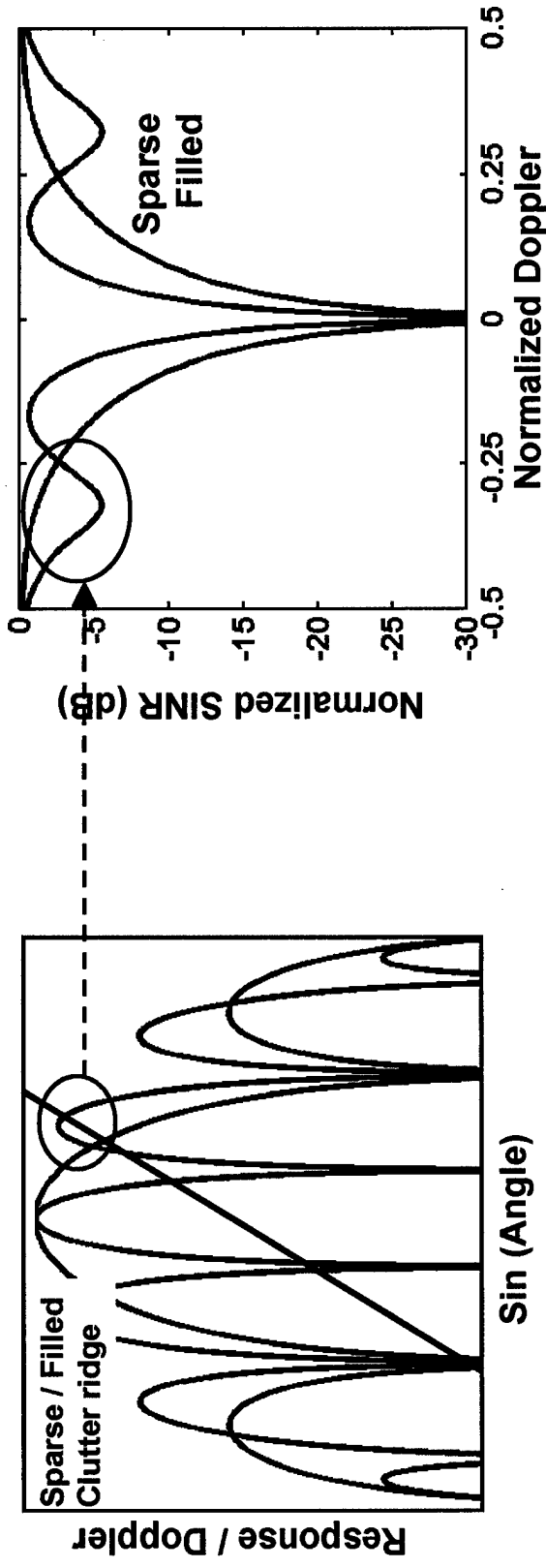
Processing Long Single Pulse Waveform



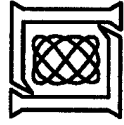
- Long single pulse radar can be made to 'appear' like a regular pulse-Doppler radar
- Looks like high PRF radar without the range ambiguities



Space Time Adaptive Processing

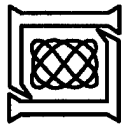


- Grating lobes lead to reduced detection performance at particular Doppler frequencies
- $$\text{SINR Loss} \approx \mathbf{v}^H \mathbf{v} - |\mathbf{v}^H \mathbf{e}|^2 = 1 - \frac{\text{Grating Lobe Gain}}{\text{Mainbeam Gain}}$$
- Should not make the array too sparse
 - For <3 dB SINR loss grating lobe gain must be 3 dB less than main lobe gain (Σ grating lobes for pulse-Doppler waveforms?)



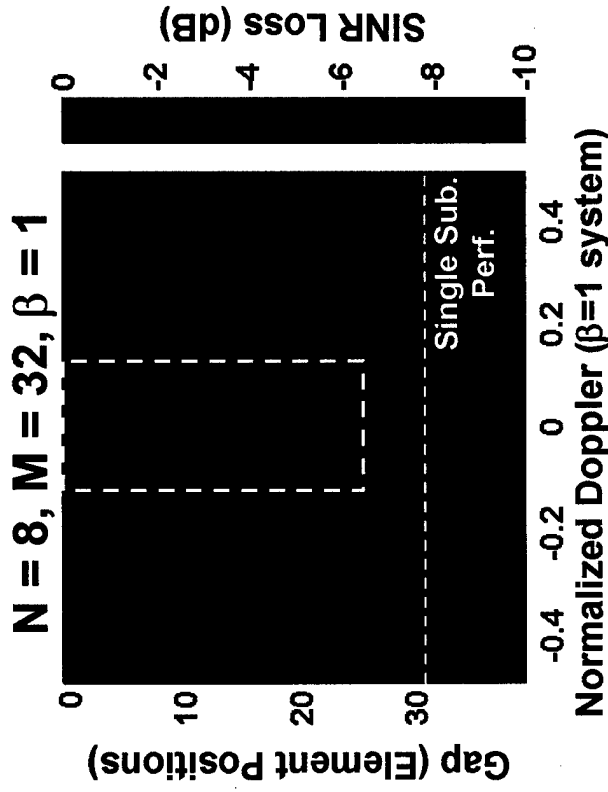
Outline

- Introduction
- Theory
- Performance
 - Dependence on waveform
 - SBR Design Example
- Summary

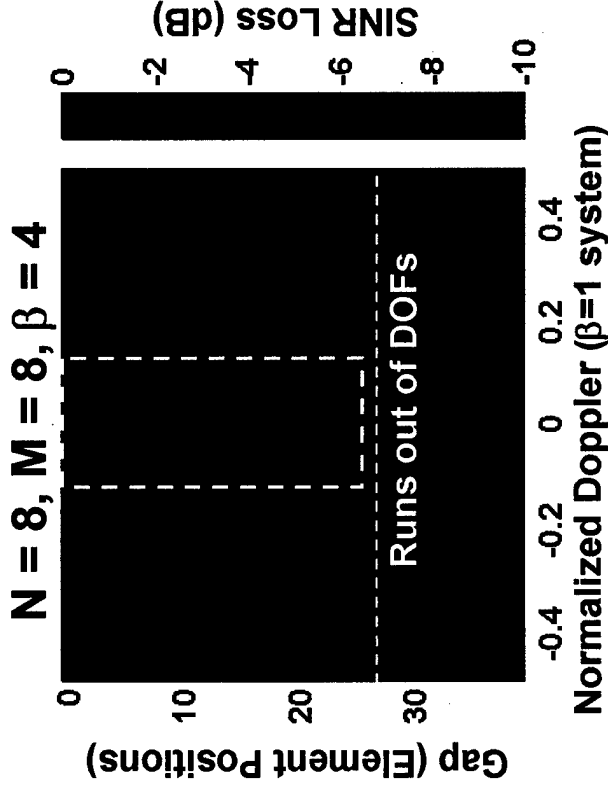


Unambiguous vs. Ambiguous Waveforms

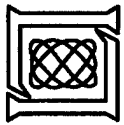
Interferometer Example



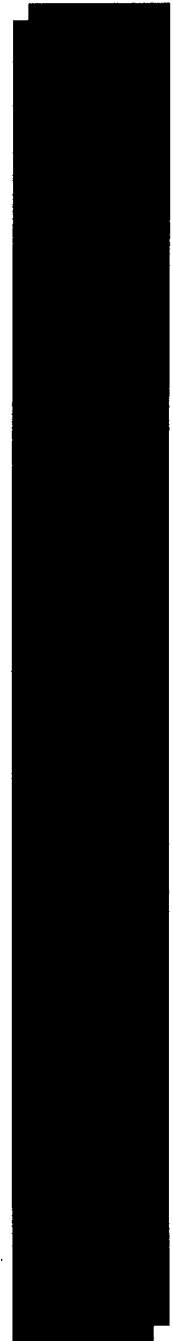
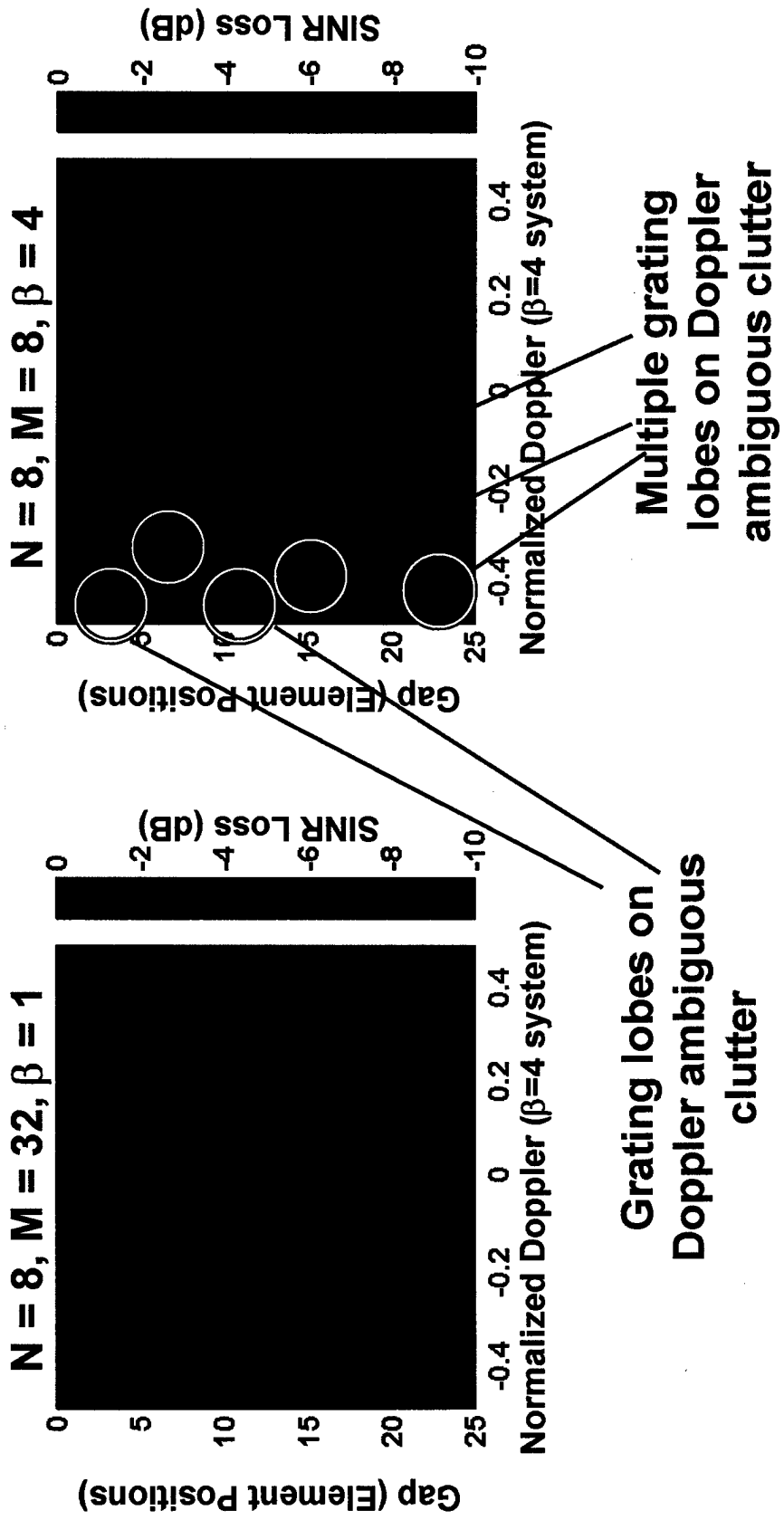
- Filled rank = $8+1(32-1)$
= 39
- Max. sparse rank = $8+2(32-1) = 70$ (reached with a 31 element gap)

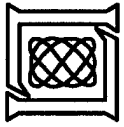


- Filled rank = $8+4(8-1)$
= 36
- Runs out of DOFs with a 27 element gap
 $8+27+2(32-1) = 63$



Unambiguous vs. Ambiguous Waveforms



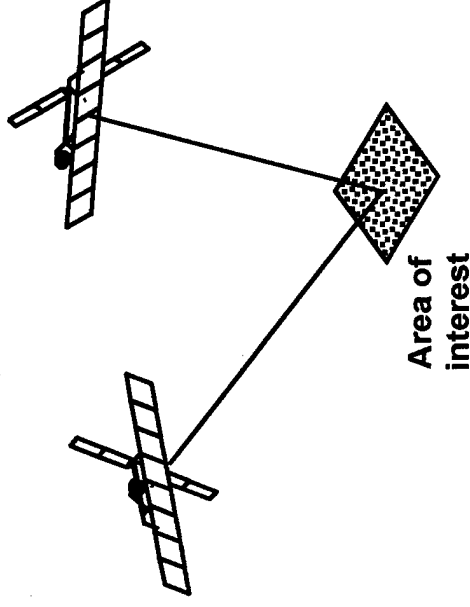


Space Based GMTI Radar Examples

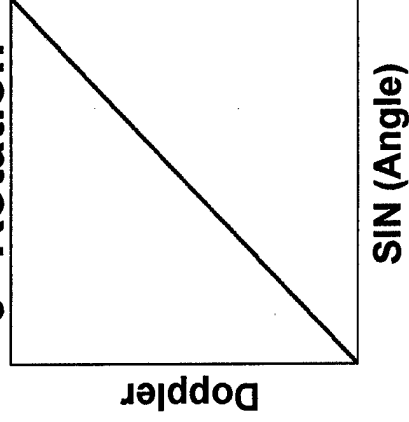
Parameters

- 32m x 2.5m filled aperture
- 10 GHz operating frequency
- 1000 km orbit
 - 7282 m/s orbital velocity
- 1 kw peak transmit power
- 200 MHz bandwidth
- Unambiguous waveform
- -12 dB const. γ clutter model
- 2500 km range
 - 16.67ms CPI length
 - Travel ~120m in a CPI

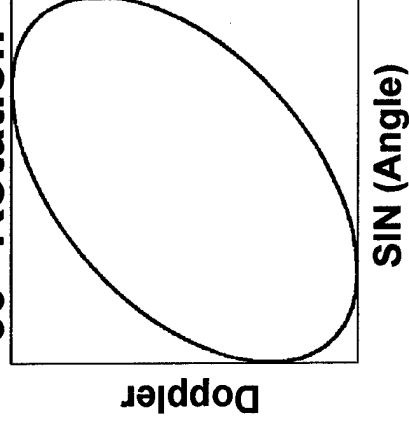
Scenarios

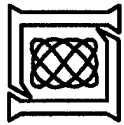


0° Rotation



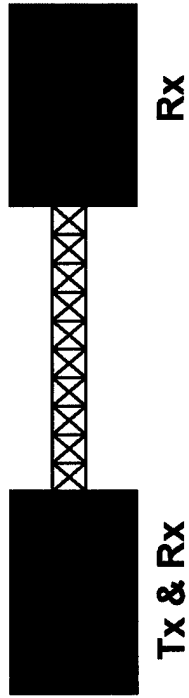
60° Rotation



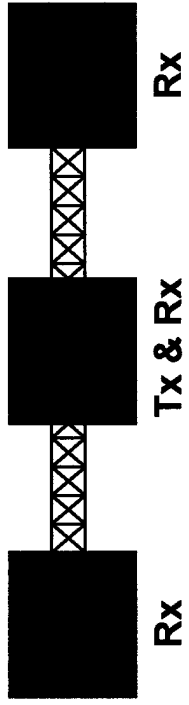


Space Based Radar GMTI Designs

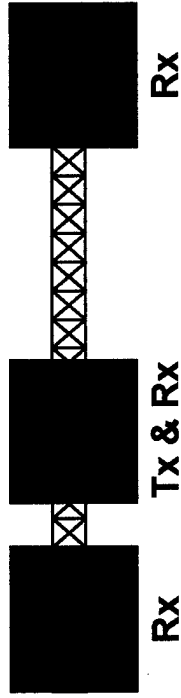
Interferometer Array



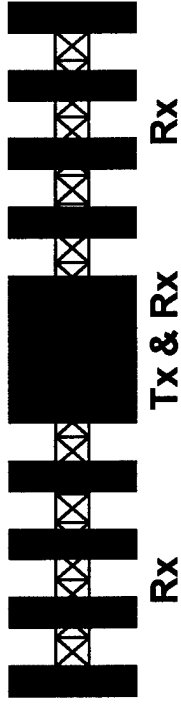
Even Spaced Equal Size



Uneven Spaced Equal Size

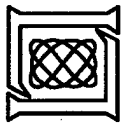


Many Apertures



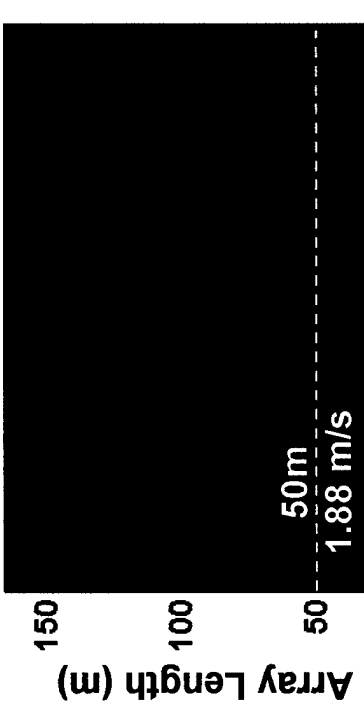
* Issues being addressed by Aerospace Corporation

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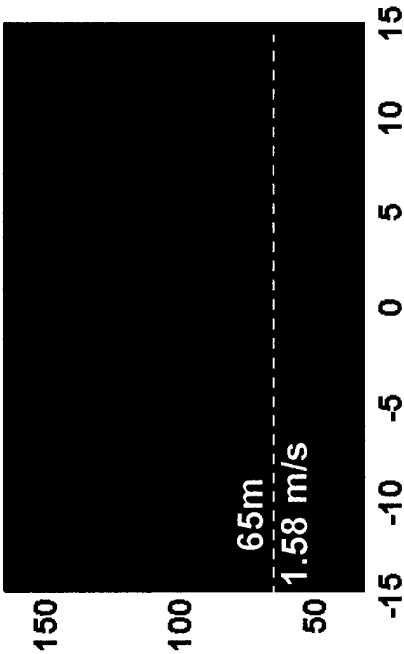


0° Rotation Scenario

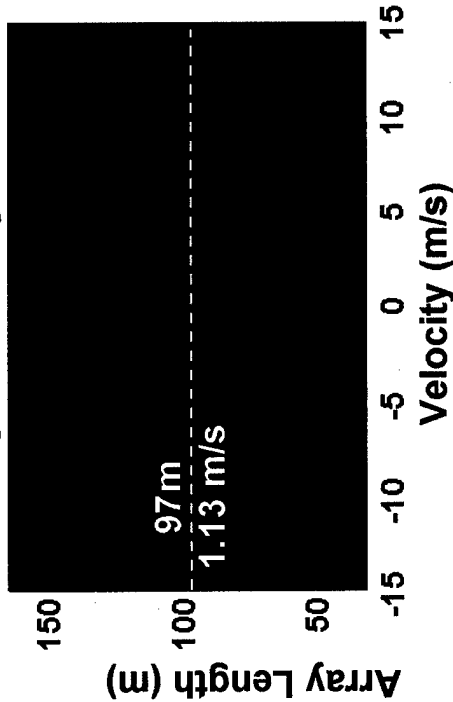
Interferometer Array



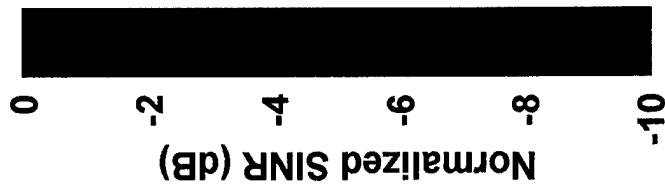
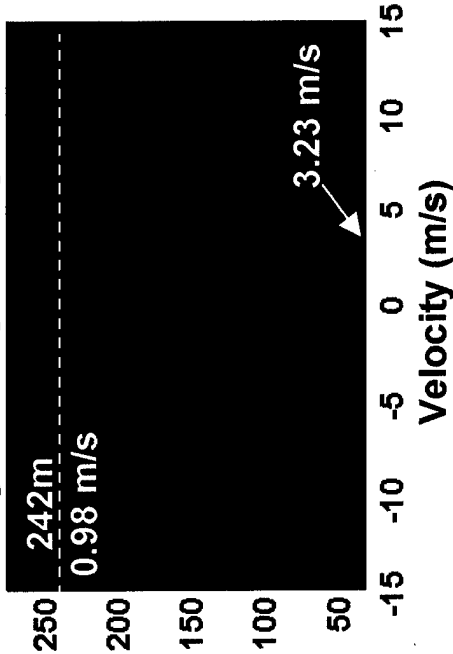
Three Equal Arrays - Even

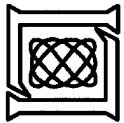


Three Equal Arrays - Uneven



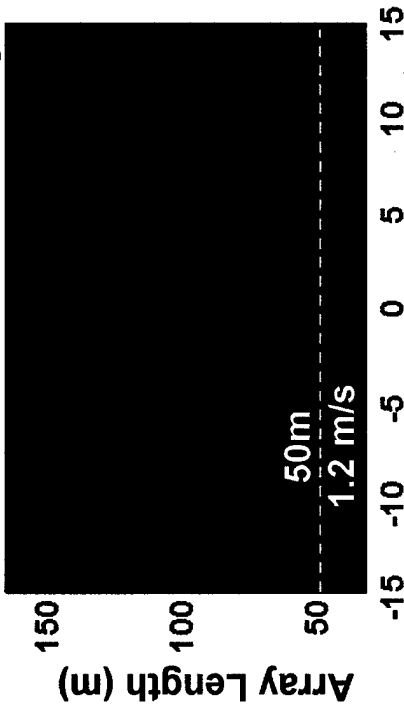
Many Unequal Apertures



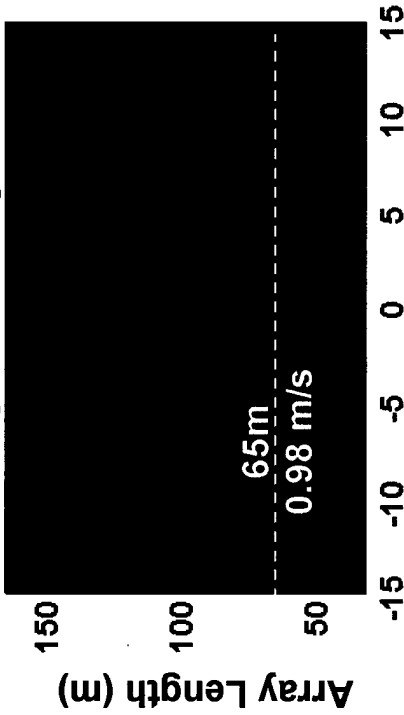


60° Rotation Scenario

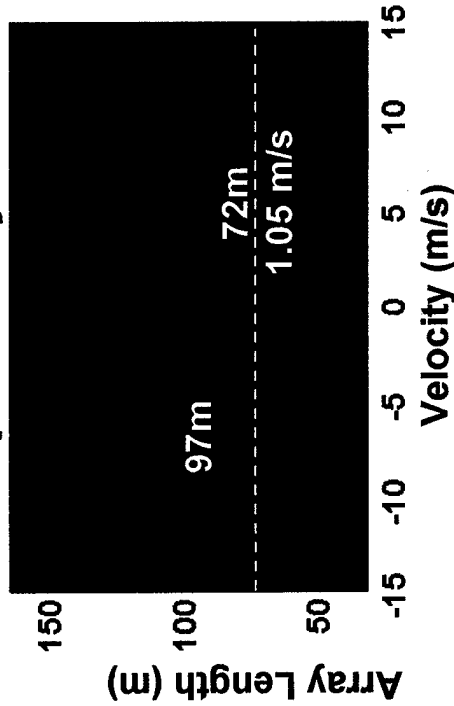
Interferometer Array



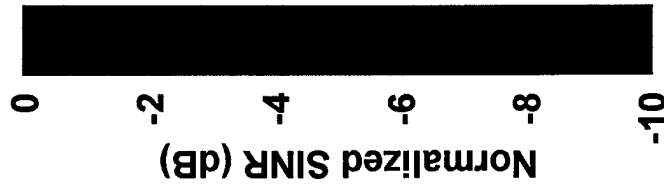
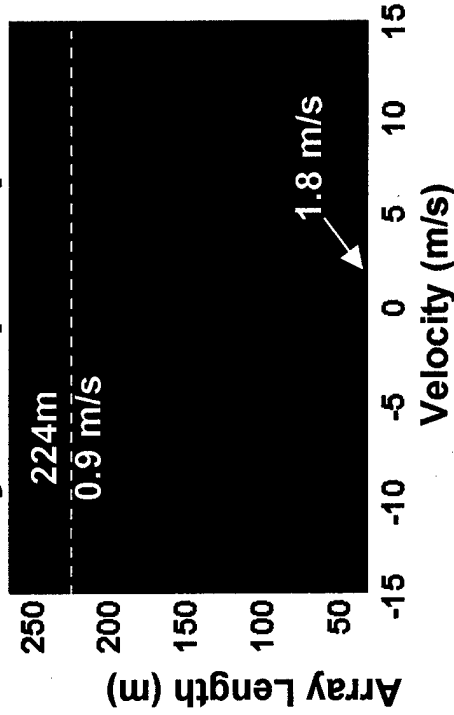
Three Equal Arrays - Even

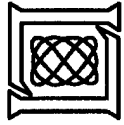


Three Equal Arrays - Uneven



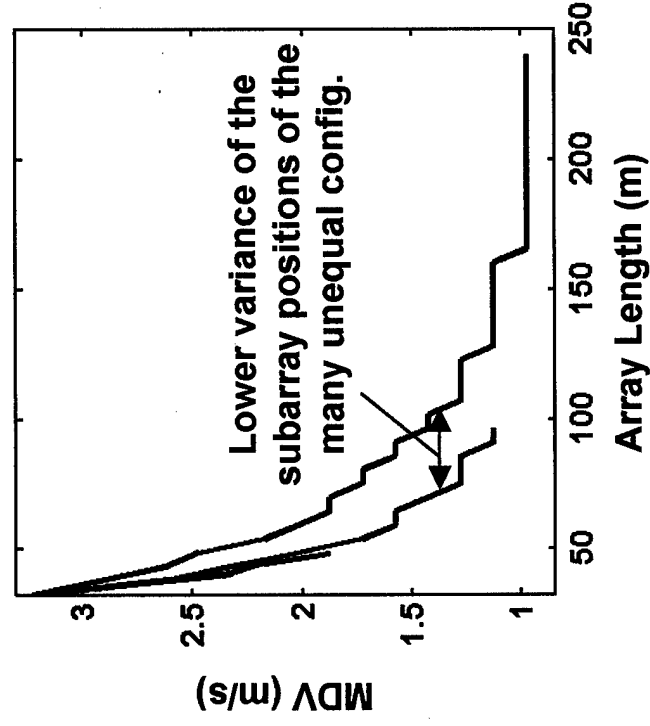
Many Unequal Apertures



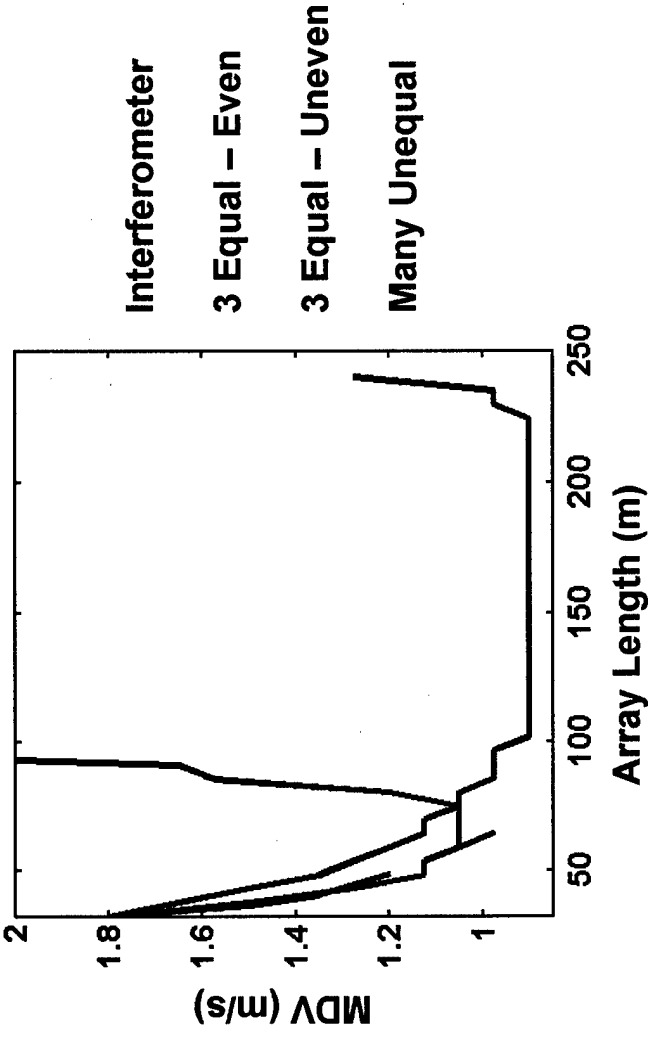


-3 dB MDV vs. Array Length

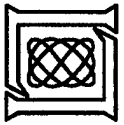
0° Rotation



60° Rotation

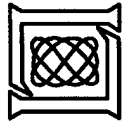


- Many unequal subarrays configuration needs a larger baseline to obtain the same performance as the other configurations, but ultimately provides the best MDV
 - 165m aperture optimizes MDV for 2500 km range
 - Longer apertures improve angle metrics

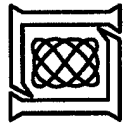


Summary

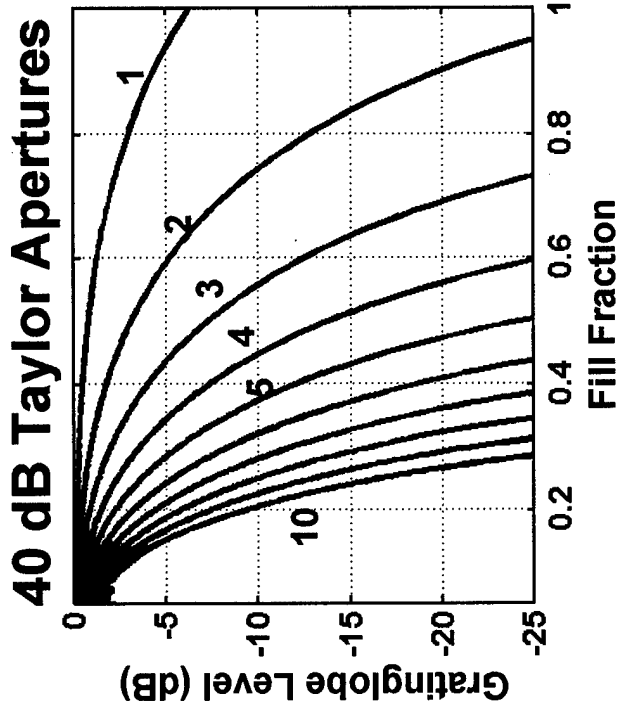
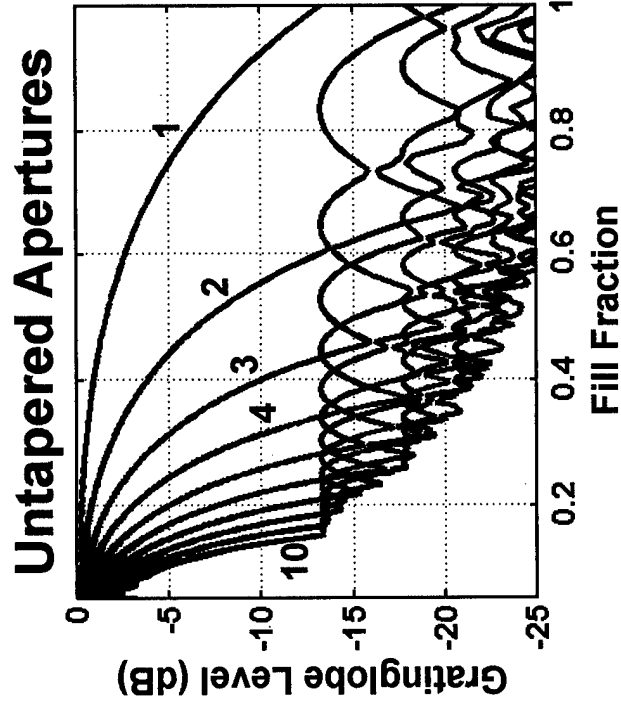
- Sparse arrays potentially improve the minimum detectable performance of space-based radars
 - Approach the MDV performance of a large filled aperture much with lower size, weight and cost
- Sparse arrays and sparse (pulse-Doppler) waveforms do not mix well
 - Sparse arrays perform well with Doppler unambiguous waveforms
 - Sparse waveforms (pulse-Doppler) perform well with filled arrays
- Long single-pulse waveforms provide range and Doppler unambiguous operation and are compatible with current STAP algorithms
- Sparse arrays with many unevenly sized unevenly spaced subarrays provide the best GMTI performance



Backup Viewgraphs

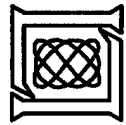


Interferometer Array Grating Lobes

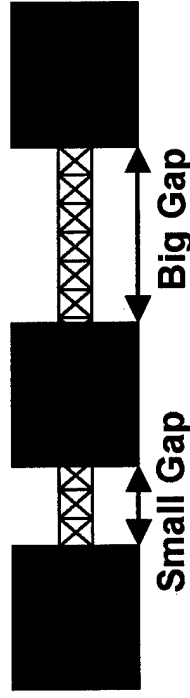
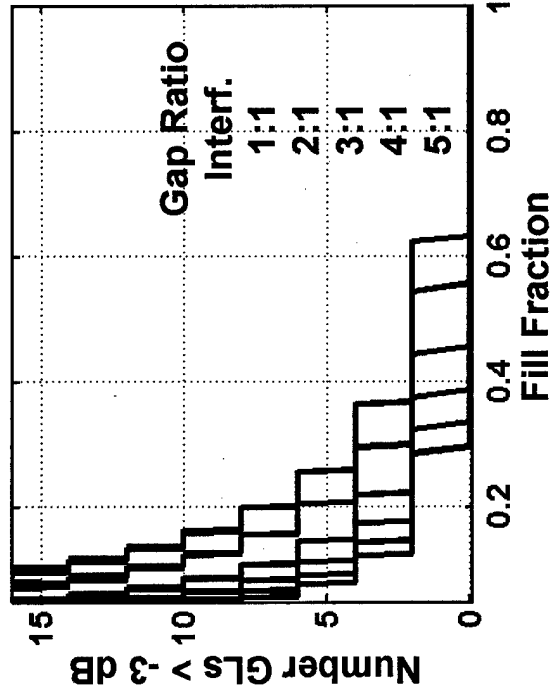
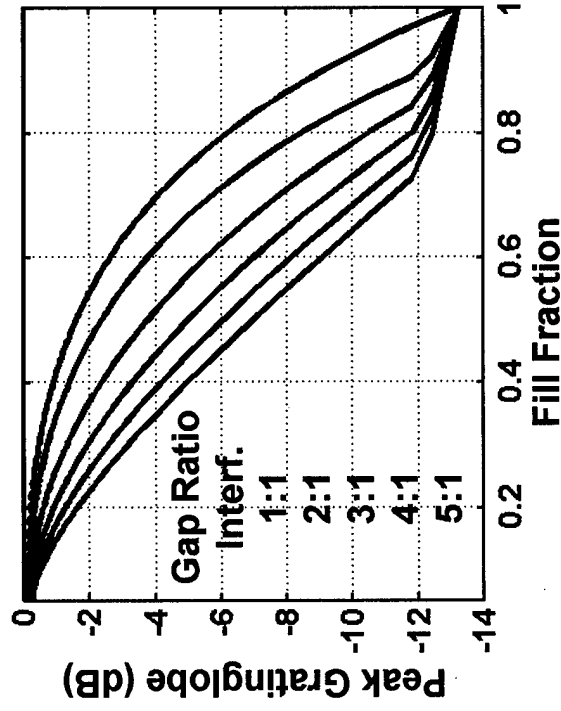


$$\text{Fill Fraction} = \frac{\text{Filled Aperture}}{\text{Total Aperture}}$$

- Grating lobes quickly appear for interferometer array
- $\sim 2/3$ fill fraction -3 dB grating lobes untapered apertures

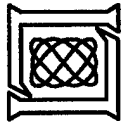


Grating Lobe Distributions 3 Equal Arrays

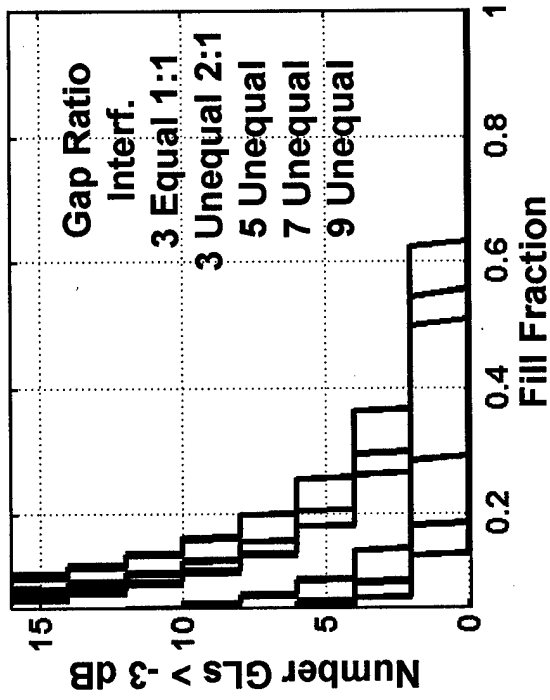
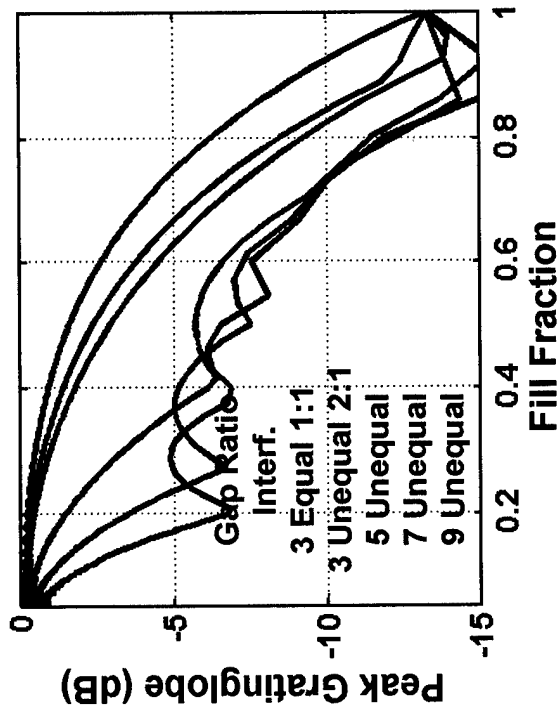


Gap Ratio = Big Gap : Small Gap

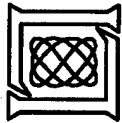
- Lower grating lobes than interferometer
- Higher gap ratios lead to lower grating lobes
 - Also poorer MDV performance



Grating Lobe Distributions Unequal Arrays

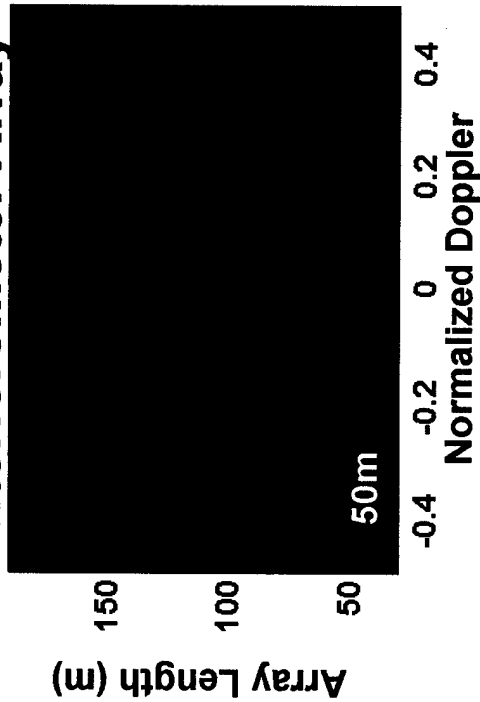


50% filled aperture in center subarray

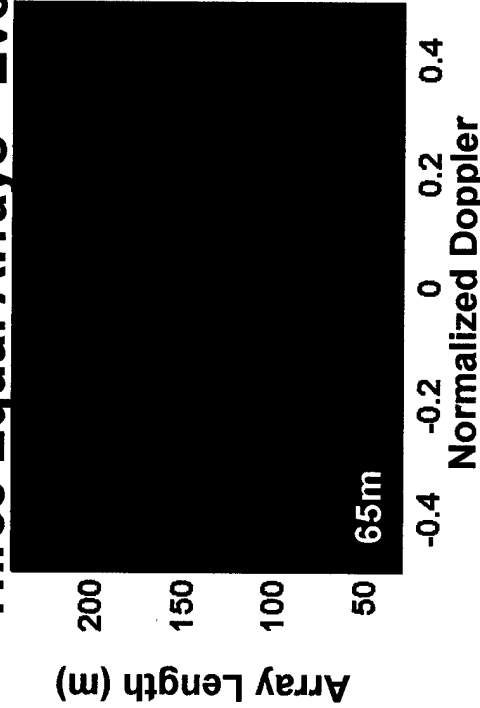


0° Rotation Scenario

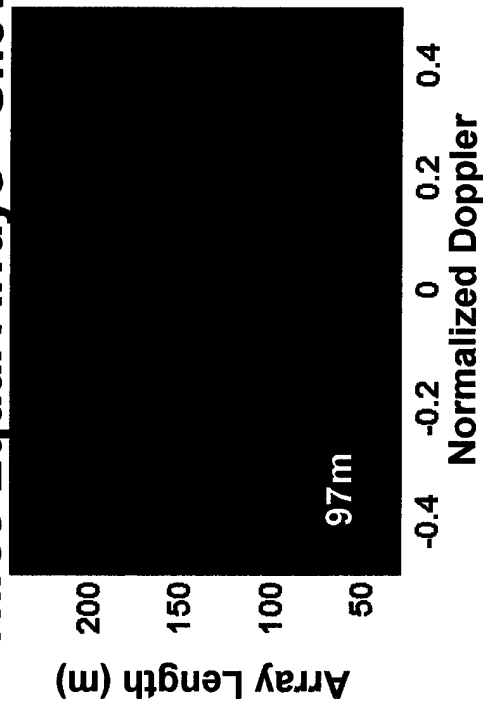
Interferometer Array



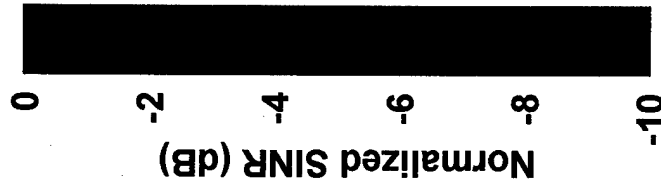
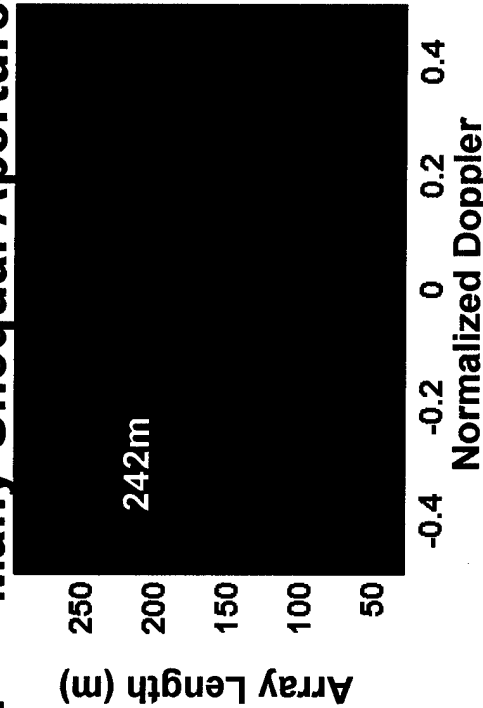
Three Equal Arrays - Even

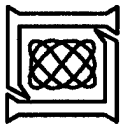


Three Equal Arrays - Uneven

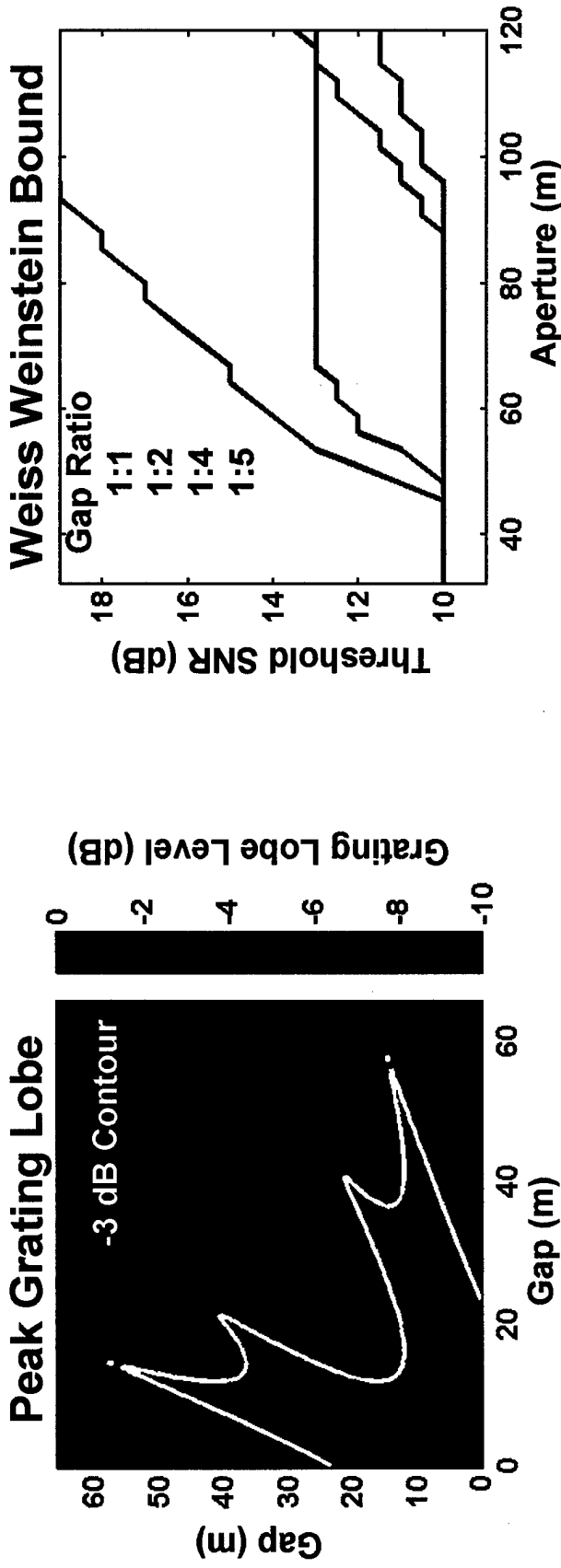


Many Unequal Apertures

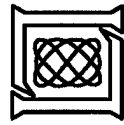




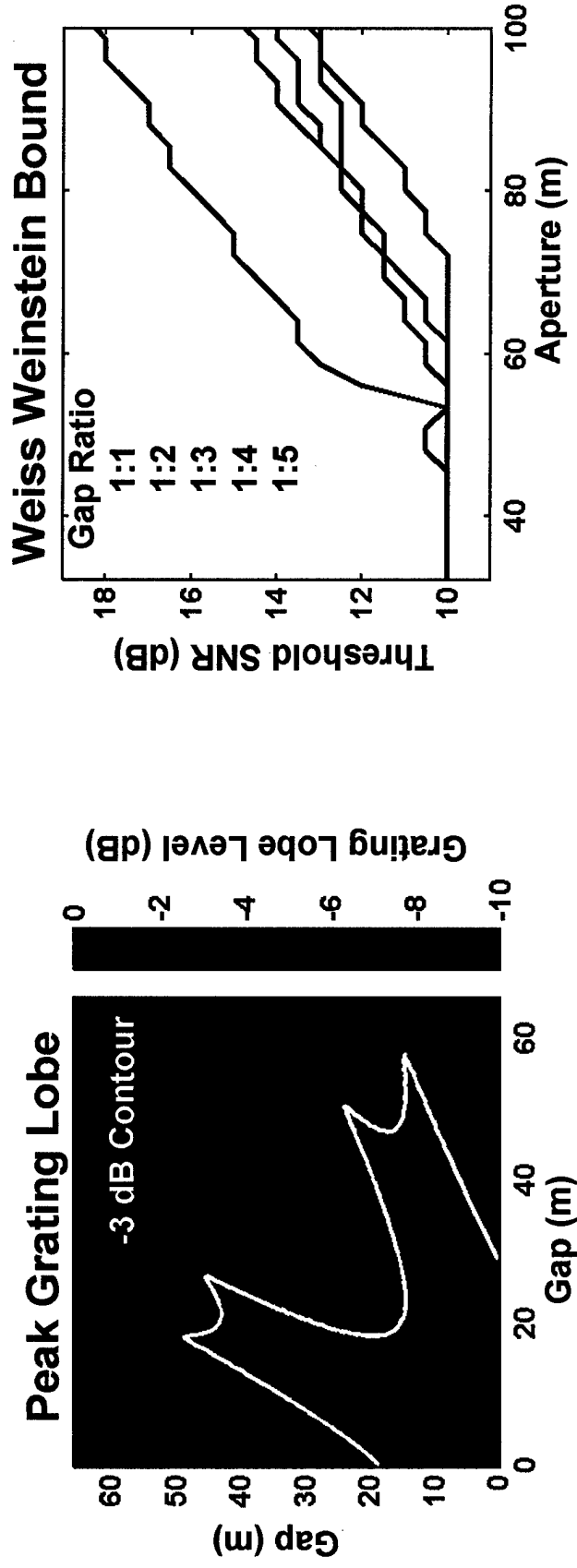
Three Equal Apertures Target Location



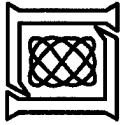
- 96 m aperture largest possible without increasing the threshold SNR
 - Provides 89 m rms error at 6° grazing
 - 82 m gives 107 m rms error



Three Unequal Apertures Target Location

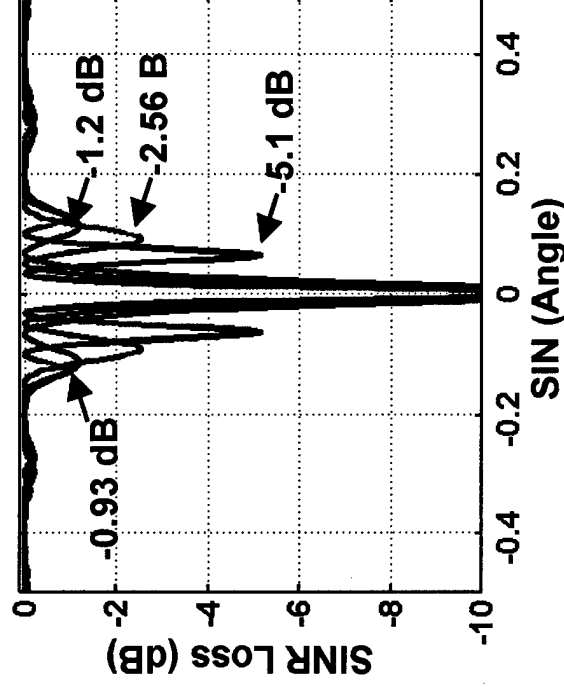
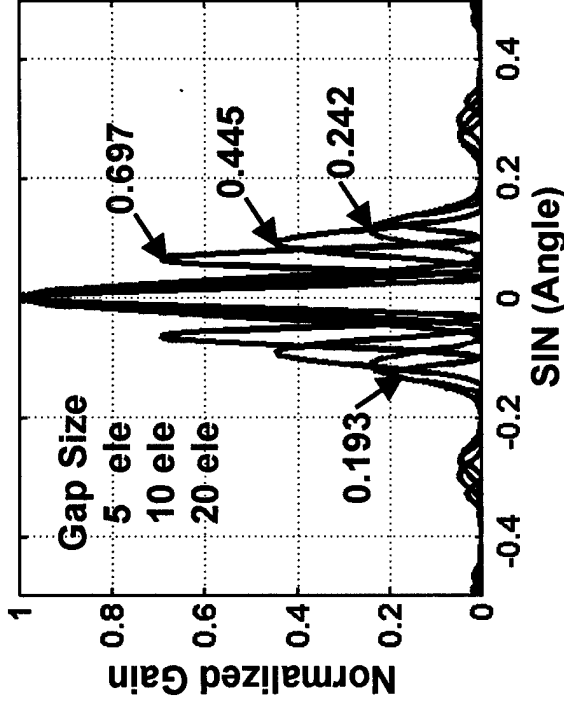


- 72 m aperture largest possible without increasing the threshold SNR
- 72m aperture Provides 119m rms error at 6° grazing



SINR Loss Due To Grating Lobe (Spatial Only Example)

20 Element Array Example



- Under the high INR assumption:

$$\text{SINR Loss} \approx \mathbf{v}^H \mathbf{v} - |\mathbf{v}^H \mathbf{e}|^2 = 1 - \frac{\text{Grating Lobe Gain}}{\text{Mainbeam Gain}}$$

- i.e., for 3 dB loss grating lobe gain (sum grating lobes for pulse-Doppler ?) must be 3 dB less than main lobe gain